

1 سبائك Co-Cr-Mo للأطراف الاصطناعية الطبية: مراجعة

- 2 اسم وكنية الباحث الاول مسبوقة صفته العلمية المختصرة (م، د، أ.د...))، اسم وكنية الباحث
3 الثاني، ٢، اسم وكنية الباحث الثالث ٣
4 ¹ الصفة العلمية، المركز البحثي أو الجامعة، التخصص الدقيق، البريد الإلكتروني (للباحثين في
5 جامعة دمشق البريد الإلكتروني الخاص بالجامعة للباحث)
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9 جامعة دمشق البريد الإلكتروني الخاص بالجامعة للباحث)
10 *توضع علامة النجمة فوق اسم الباحث الذي تتم المراسلات معه بغض النظر عن الترقيم او ترتيب
11 الاسماء (كباحث رئيسي - طالب دراسات عليا)
12

13 الملخص:

- 14 يقدم المقال دراسة مرجعية لسبائك Co-Cr-Mo المستخدمة في الطب لتصنيع الأطراف الاصطناعية.
15 يتم النظر في التركيبات الأساسية للسبائك من هذا النوع، وكذلك البنية المجهرية وخصائصها. يتم
16 التطرق إلى مسائل التصنيع عن طريق الصب وكذلك طرق المعالجة الحرارية للمنتجات الطبية. وقد
17 وجد أن استخدام المعالجة الحرارية يسمح بالحصول على البنية المجهرية اللازمة، وكذلك زيادة
18 خصائص القوة. بالإضافة إلى ذلك، تم النظر في طرق تشطيب الأجهزة الطبية التي تساهم في تحسين
الخصائص الاحتكاك.

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Co-Cr-Mo Alloys for Medical Endoprostheses: Review

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Abstract:

The article presents a literature review of Co-Cr-Mo alloys used in medicine for the manufacture of endoprostheses. The basic compositions of alloys of this type, as well as microstructure and their properties are considered. The questions of manufacturing by casting as well as methods of heat treatment of medical products are touched upon. It was found that the use of heat treatment allows to obtain the necessary microstructure, as well as to increase the strength properties. In addition, the methods of finishing of medical devices, which contribute to the improvement of tribological properties, were considered.

Keywords: Co-Cr-Mo alloys, Endoprostheses, Composition, Microstructure, Mechanical properties, Medical applications, Heat treatment, Finishing treatment, Surface treatment.



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55 1. Introduction:

56 An actual direction of scientific search for new
57 metal-based materials is the research devoted to the
58 development of promising alloys for the production
59 of medical devices. In Belarus, the medical industry
60 is developing quite intensively, but in some of its
61 segments there is a certain deficit of domestic
62 products. Institutions are forced to purchase
63 imported products, while all operating costs are tied
64 to the foreign supplier (service, consumables). The
65 lack of necessary products and equipment for
66 traumatology, orthopedics and prosthetics
67 significantly reduces the number of medical
68 operations that can be performed annually by
69 Belarusian specialists, which makes it impossible to
70 fully provide those in need with appropriate
71 treatment.

72 Endoprostheses are artificial bioimplants that
73 provide restoration of the function of lost or damaged
74 articular bone surfaces in patients with degenerative
75 diseases and trauma consequences. Nowadays
76 various classes of materials are used for their
77 manufacturing: metal, polymeric, ceramic and
78 composite materials, which function in biological
79 media with different physical and chemical nature,
80 and the solution of problems of their biochemical and
81 mechanical interaction with organic tissues and bone
82 material is a complex task of interdisciplinary
83 fundamental research at the intersection of metal
84 science and thermal processing of materials, biology
85 and medicine. At the same time, in case of partial or
86 complete loss of the implant performance, repeated
87 surgical intervention is required to restore the
88 functionality of the life support system of the
89 organism.

90 One of the most widely used metal materials for
91 medical applications are alloys based on the Co-Cr-
92 Mo system due to their unique combination of the
93 above mentioned properties for implant
94 manufacturing. High corrosion resistance is achieved
95 due to a thin surface oxide layer consisting mainly of
96 chromium oxide with a small content of
97 molybdenum oxides.

98 In addition, the establishment of the main factors
99 determining the processes of structure formation and

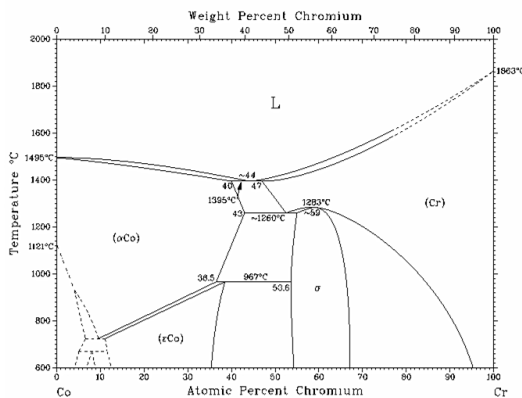
100 surface modification of metallic materials based on
101 Co-Cr-Mo system is important for the development
102 of Belarusian production of endoprostheses with
103 high physical and mechanical, operational
104 characteristics and biocompatibility for use in the
105 field of traumatology and orthopedics.

106 2. Compositions, structures and 107 properties of materials used for 108 medical devices (endoprostheses)

109 It is recommended to use Co-Cr-Mo alloy for
110 manufacturing many biomedical implants, which
111 should have good tribological properties (Hashmi e at
112 al., 2023).

113 The composition of Co-based biomedical alloys is
114 usually divided into two types. One of them is Co-
115 Cr-Mo alloy containing 5-7 % Mo and 27-30 % Cr.
116 This material has been in use for more than 20 years
117 and is increasingly used as the main material for
118 bioimplants (Hashmi e at al., 2023; Silva e at al., 2023;
119 Chen e at al., 2015; Patel e at al., 2012). Another type of
120 cobalt alloy is Co-Ni-Cr-Mo consisting of Ni (33-37
121 %), Cr (19-21 %) and Mo (9-11 %). Compared to Co-
122 Cr-Mo, it was used in the biomedical field later and
123 found its application in the creation of highly loaded
124 joints, including prosthetic legs (Patel e at al., 2012;
125 Alvarado e at al., 2003). According to a number of
126 studies, cobalt alloys have been found to be highly
127 biocompatible and particularly resistant to corrosion
128 even under conditions of high chloride content. It is
129 believed that these properties are due to the presence
130 of passive oxide layers spontaneously growing on the
131 alloy surface. In a corrosive environment, these
132 layers act as barriers and prevent corrosion (Chen e at
133 al., 2015; Alvarado e at al., 2003; Evans, e at al., 1986;
134 Öztürk e at al., 2006; Ramsden e at al., 2007).

135 Figure 1 shows the phase diagram of the state of
136 alloys based on the Co-Cr system, which are used for
137 the manufacture of endoprostheses depending on the
138 peculiarities of the human body, its individual
139 characteristics and other criteria. Molybdenum,
140 nickel, titanium and other elements serve as the main
141 alloying elements of such alloys (Wahi e at al., 2016).



142
143 Figure 1 - Phase diagram of state of Co-Cr-based alloys
144 (Ramsden e at al., 2007).

145 The studies (Hashmi e at al., 2023; Hiromoto e at al.,
146 2005) considered alloys with different Ni content:
147 low Co-29Cr-(6, 8)Mo (wt. %) and ordinary Co-
148 29Cr-6Mo-1Ni (ASTM F75-92). The main purpose
149 of these works was to study the alloys for corrosion
150 resistance in the environment close to human and to
151 study the effect of Ni on the human body, the high
152 content of which can cause allergic reactions
153 (Hiromoto e at al., 2005; Thyssen e at al., 2007). As a
154 result, an alloy based on Co-Cr-Mo with low Ni
155 content ~ 0.03 (wt. %) was obtained. At the same
156 time, the decrease in Ni content contributed to a
157 decrease in ductility. In order to neutralize this effect,
158 it was decided to reduce the grain size by using die
159 forging (Hiromoto e at al., 2005).

160 The authors' research (Liao e at al., 2012; Jenko e at al.,
161 2018; Giacchi e at al., 2018) was aimed at studying the
162 microstructure of cobalt-based alloy (Co-Cr-Mo)
163 under cast and deformed conditions. The aim of this
164 research was to obtain additional information about
165 the microstructure of Co-Cr-Mo based alloys by
166 identifying different phases and morphologies and
167 evaluating their possible transformation during
168 solidification and cooling under industrial
169 conditions. Table 1 presents information on the
170 compositions investigated in the works (Jenko e at al.,
171 2018; Giacchi e at al., 2018).

172 Co-Cr-Mo based alloys combine face-centered cubic
173 (FCC) and hexagonal close-packed (HCP) crystal
174 structures. It is noted that at room temperature the
175 predominant phase is (FCC). It is noted that the

176 transition of one phase to another ((FCC → HCP) can
177 be realized either isothermally or by deformation
178 (Balagna e at al., 2012). In addition, the [C] present in
179 the alloys contributes to the formation of carbides,
180 the size and distribution of which is significantly
181 influenced by the technological process. After
182 casting and heat treatment provided by the
183 technological process, various solid phases such as
184 $M_{23}C_6$ (M=Cr, Mo, Co), M_7C_3 appear. In the works
185 aimed at investigating the microstructure of Co-
186 28Cr-6Mo (Fellah e at al., 2023; Efremenko e at al.,
187 2023; Roudnicka e at al., 2021; Roudnická e at al., 2021;
188 Murr e at al., 2011) and Co-29Cr-6Mo [21] foundry
189 alloys, it is noted that through heat treatment the
190 original cellular structure (72 %FCC-28 %GPU)
191 disappears and it is replaced by σ -type intermetallic
192 phases (Mo-, Co- and Si-type phases) (Fellah e at al.,
193 2023; Efremenko e at al., 2023; Roudnicka e at al., 2021;
194 Roudnická e at al., 2021; Murr e at al., 2011). It is noted
195 that intermetallic and eutectic carbides have similar
196 size. Their presence in the microstructure of Co-Cr-
197 Mo-based alloys has a positive effect on the
198 properties of endoprostheses: they contribute to the
199 increase in strength. It is also noted that under the
200 influence of heat treatment or in the presence of
201 nitrogen, carbides of the $M_{23}C_6$ type form carbides of
202 the M_6C type. They are located at grain boundaries
203 and are smaller in size than $M_{23}C_6$ carbides (Liao e at
204 al., 2012; Jenko e at al., 2018; Ghalme e at al., 2016).

205 In (Ghalme e at al., 2016) it is proposed to add 2-6 wt.
206 % Ti in Co-Cr-Mo alloy. At the same time, carbides
207 Cr_7C_3 and $Cr_{23}C_6$ were noticed along the grain
208 boundaries, as well as phases α -Co, ϵ -Co, β -Ti,
209 $CoTi_2$.

210 Orthopedic implants made of Co-Cr-Mo alloys,
211 which perform the function of bones to replace the
212 failed hard tissues, usually operate under cyclic loads
213 under living conditions (Atkinson e at al., 1980; Devine
214 e at al., 1972; Niinomi e at al., 2002; Mani e at al., 2011).
215 The reliability of such implants after insertion is
216 largely determined by their strength and fracture
217 toughness. Fatigue failure is one of the major
218 problems leading to loosening and ultimate failure of
219 implants (Niinomi e at al., 2007; Teoh e at al., 2000).
220 Artificial joints made of Co-Cr-Mo alloys are now

221 increasingly used in younger and more active
222 patients, where the service life is significantly longer
223 under more severe operating conditions. Therefore,
224 the evaluation and improvement of mechanical
225 properties of alloys used for the fabrication of metal
226 elements of hip arthroplasties are becoming more
227 and more of an issue (Wei e at al., 2018).

228 **Table 1 - Composition of Co-Cr-based alloys studied**
229 **in the works (Jenko e at al., 2018; Giacchi e at al.,**
230 **2018)**

Article, №	Content of main components in the alloy								
	Alloy	Cr	Co	Mo	Mn	Fe	Si	C	W
Jenko e at al., 2018	Co-Cr-Mo	0,28	63,9	6,4	0,36	0,30	0,73	-	-
	C1	30,60	60,75	6,14	-	-	1,29	0,13	0,36
	C2	28,93	62,99	5,83	-	-	1,05	≤0,021	0,38
	C3	27,01	64,13	6,30	-	-	1,08	≤0,021	0,40
Giacchi e at al., 2018	ASTM F75 (standard)	27,0-30,0	59,0-69,0	5,0-7,0	-	-	To 1	To 0,35	To 0,2

235 It should be noted that when casting Co-Cr-based
236 alloys as a result of crystallization, large dendritic
237 grains are formed, the presence of which reduces the
238 yield strength of the alloy and promotes the
239 appearance of defects such as inclusions and
240 micropores, which increase internal stresses (Fellah e
241 at al., 2019). However, research in this area continues,
242 and one option to solve this problem is the use of
243 special types of casting followed by heat treatment.
244 In the last few decades, Co-Cr-Mo (F75) casting
245 alloy has been used for the fabrication of orthopedic
246 implants by casting (Fellah e at al., 2019; Nalbant e at
247 al., 2007).

248 In (Okazaki e at al., 2008; Lee e at al., 2005) the
249 influence of annealing and hot forging on the
250 microstructure and mechanical properties of Co-Cr-
251 Mo alloy was investigated in order to obtain initial
252 data for the development of a new forging process.
253 The Co-Cr-Mo alloy was obtained by vacuum
254 induction melting. The Co-Cr-Mo alloy ingot was
255 first homogenized at 1250 °C for 5 h. A part of the
256 homogenized ingot was aged at 1200 °C for 1 h,
257 followed by hot forging in the form of 30 mm
258 diameter rod samples. The rod specimens were
259 reheated at 1200 °C for 1 h and hot forged as 20 mm
260 diameter rods. The samples were then annealed at
261 1200 °C for 1 h and then cooled in air. The other part
262 of the homogenized alloy was hot forged into 42 mm
263 diameter rod samples after being annealed at 1200 °C
264 for 1 h and hot forged into 42 mm diameter rod
265 samples. Some of them were heat-treated by holding
266 at 1100 °C for 1 h followed by hot forging to reduce
267 the area of the investigated samples by 40%, 42%,
268 47%, 49% and 57%, respectively. To investigate the
269 effect of heating temperature on microstructure, one
270 of the rod samples was annealed at 1000 °C for 1 h
271 and hot forged to reduce the area by 50% at an initial
272 temperature of 1000 °C. In this way, annealed and hot
273 forged Co-Cr-Mo alloys were obtained for
274 microstructural studies and mechanical tests. As a
275 result, it was found that a large number of precipitates
276 were observed at the grain boundary of the annealed
277 Co-Cr-Mo alloy, which was attributed to the
278 relatively high carbon content. In addition, the hot-

231
232 **3. Processes of vacuum casting and**
233 **heat treatment of metal**
234 **bioimplants**

279 annealed Co-Cr-Mo alloy had a finer structure than
280 the annealed Co-Cr-Mo alloy (Okazaki e at al., 2008).

281 It is mentioned in (Alvarado e at al., 2003) that casting
282 as a method of manufacturing Co-Cr-Mo-based alloy
283 endoprostheses on a commercial scale is widely
284 used. It is also noted that the technology of
285 endoprosthesis fabrication by casting requires faster
286 processing time than, for example, the fabrication of
287 bioimplants by forging. The research results obtained
288 in this work have shown that both forged and cast Co-
289 based alloy endoprostheses have high corrosion
290 resistance and abrasion resistance. It is especially
291 noted that cast medical devices made of this type of
292 alloys have finer crystals than those obtained by
293 forging, which has a positive effect on the properties
294 of the obtained hip joints (Balagna e at al., 2012).

295 The authors of (Chen e at al., 2017) investigated the
296 influence of carbon content in Co-Cr-Mo-based
297 alloys on wear resistance. Samples (hip joint
298 simulators) were made of Co-Cr-Mo alloy by
299 vacuum induction melting. As a result, no significant
300 difference in wear loss of Co-Cr-Mo alloys with low
301 and high carbon content was found.

302 In (Cawley e at al., 2003), the Co-Cr-Mo alloy in
303 different states was studied in detail: cast, heat-
304 treated (HT), obtained by hot isostatic pressing
305 (HIP), HIP followed by HT, obtained by sintering
306 followed by HT and HIP) and concluded that the cast
307 version has the highest wear resistance due to the
308 high volume fraction of carbides.

309 The study (Roudnicka e at al., 2021; Takaichi e at al.,
310 2019) compares Co-Cr-Mo alloy endoprostheses
311 produced by investment casting and the material
312 obtained by advanced 3D printing technology. The
313 first set of results shows the different response of
314 both materials to the hardness increase during
315 annealing at increasing temperatures up to the
316 transformation temperature. Based on these results,
317 solution treatment and subsequent aging under
318 conditions to achieve maximum hardness was
319 applied

320 The work (Tonelli e at al., 2023) aimed to investigate
321 the heat treatment of LPBF Co28Cr6Mo alloy (based

322 on selective melting of subsequent layers of metal
323 powders) by direct aging performed in the range of
324 600-900 °C for 180 minutes. The effects on the
325 hardness and microstructural characteristics of the
326 heat-treated alloys were also emphasized to
327 investigate. In this case, it was found that soaking at
328 850 °C for 180 minutes followed by aging was the
329 most optimal heat treatment method. Equally
330 important was the dry sliding wear of the fabricated
331 and heat-treated LPBF Co-28Cr-6Mo alloy,
332 considering the conventional deformed alloy as a
333 reference. Under test conditions close to the
334 operational test conditions, the fabricated LPBF
335 alloy showed wear resistance higher than that of the
336 conventional deformed alloy. Optimized aging
337 treatment significantly modified the finished LPBF
338 microstructure, improved the hardness of the alloy
339 and, in general, had a positive effect on its friction
340 and wear resistance.

341 It is also noted that, as a rule, a conventional Co-Cr-
342 Mo cast alloy is subjected to high temperature
343 treatment at 1230 °C with a special solution followed
344 by quenching (Tonelli e at al., 2023).

345 In (Mantrala e at al., 2015), a Co-Cr-Mo cast alloy was
346 investigated by heat treating at 1200 °C for 30, 45
347 and 60 min, followed by quenching in water followed
348 by isothermal aging at 850 °C for 2, 4 and 6 hours.
349 The heat-treated samples were evaluated for
350 microstructure, hardness, wear resistance and
351 corrosion resistance. The results showed that the
352 highest hardness of 512 ± 58 Hv and wear rate of
353 $0,90 \pm 0,14 \times 10^{-4}$ mm³/N-m could be achieved by
354 appropriate heat treatment after fabrication.

355 **4. Finishing processes of metal** 356 **elements of hip joint** 357 **endoprostheses**

358 One of the most important requirements for metal
359 elements of hip joints are surface quality and
360 dimensional accuracy, where one of the main
361 indicators of surface quality is its roughness. Surface
362 roughness is of great importance for functional
363 properties such as, for example, wear resistance. As

364 a result, it also determines the quality of the
365 endoprosthesis itself.

366 It is noted in (Döbberthin e at al., 2020) that
367 dimensional and shape accuracy are important
368 aspects that can be controlled by selecting suitable
369 machining processes. This paper presents an
370 experimental analysis of shape accuracy in
371 electrochemical (EC) polishing of femoral heads for
372 hip arthroplasties. Femoral heads were pre-treated by
373 barrel and drag grinding. The accuracy of the shape
374 obtained after EC-polishing was evaluated by the
375 authors taking into account the pretreatment
376 processes. It is observed that EC polishing is a
377 common process for surface smoothing of metallic
378 materials. This method is based on anodic dissolution
379 of metal. Like electrochemical machining, EC
380 polishing is carried out with a power source and
381 electrolyte between the cathode and anode. In
382 contrast to mold removal, EC polishing uses a bath
383 of electrolyte and current densities in the range of 0.4
384 to 3 A/cm². For this method, the workpiece is
385 clamped on a movable holder and immersed in an
386 electrolyte bath. According to the principle of the
387 process, the entire surface of the anode is practically
388 surface-removed. As a consequence, the roughness
389 peaks are reduced and the edges and cracks are
390 smoothed out. The advantages of using this method
391 are also mentioned: compared to grinding, EC
392 polishing produces less heat exchange with the
393 workpiece surface and therefore ensures that the
394 boundary layer is not influenced. A second advantage
395 of using this method is that, limited only by the
396 volume of the electrolyte bath, workpieces of
397 different shapes and configurations can be machined.
398 In addition, this method is highly efficient, which is
399 due to the ability to treat the surface of the
400 workpieces in a relatively short polishing time, as
401 well as the possibility of simultaneous polishing of
402 several workpieces, which allows the use of this
403 method of surface treatment on an industrial scale.

404 The papers (Chu e at al., 2002; Sodhi e at al.,1996;
405 Sioshansi e at al., 1987; Hegemann e at al., 2001; Quinet
406 e at al., 1992) review plasma surface modification
407 (PSM), which is an efficient and economical method
408 for surface treatment of many materials and is of

409 increasing interest in biomedical engineering. The
410 articles review various common plasma technologies
411 and experimental techniques used for the study of
412 biomedical materials such as plasma spraying and
413 etching, plasma implantation, plasma deposition,
414 plasma polymerization, laser plasma deposition,
415 plasma sputtering, etc. The unique advantage of
416 plasma modification is that surface properties and
417 biocompatibility can be improved locally without
418 changing the basic properties of materials. Solid
419 tissue substitutes, blood contact prostheses,
420 ophthalmic devices and other medical devices have
421 been considered as research samples. Using RPM as
422 an economical and effective method of materials
423 processing, it is possible to change the chemical
424 composition and such properties as wettability,
425 colorability, hardness, chemical inertness,
426 biocompatibility of the materials surface, etc. in a
427 continuous mode.

428 In (Wei e at al., 2016; Wang e at al., 2013; Mattei e at al.,
429 2011; Gao e at al., 2012; Chyr e at al., 2014), the
430 possibility of using laser interference lithography
431 (LIL) to modify the surface of implantable Co-Cr-
432 Mo alloy, which is universally used as a material for
433 artificial joints in total endoprosthetics, is
434 investigated. Experimental results show that the
435 surface of samples modified by laser interference
436 lithography has better tribological characteristics and
437 hardness compared with untreated materials,
438 including a 64 % reduction in the coefficient of
439 friction and a 40 % increase in hardness, which is
440 very promising for significantly reducing the average
441 revision rate after primary total hip arthroplasty in
442 the future. The results of Co-Cr-Mo alloy surface
443 texture study (Wang e at al., 2013) showed that the
444 petal-like surface texture can effectively reduce the
445 friction and wear of Co-Cr-Mo artificial joints. In
446 (Mattei e at al., 2011), they investigated surface
447 texturing to modify the friction surface by electrical
448 discharge etching to improve lubrication and found
449 that the lubrication properties could be improved in
450 pin-on-disk type experiments.

451 Researchers in (Gao e at al., 2012) studied the
452 tribological effects of micro dimpled surface
453 texturing for its application in ceramic-on-ceramic

454 hip prostheses. Dimpled textures on ceramic surfaces
 455 were fabricated by microdrilling on CNC machines.
 456 Compared to surfaces without dimples, dimpled
 457 surfaces with high density and large dimple sizes
 458 showed a significant increase in tribological
 459 properties: friction was reduced by 22% and wear by
 460 53%.

461 In (Chyr e at al., 2014), the possibility of using laser
 462 interference lithography to modify the surface of Co-
 463 Cr-Mo implantation alloy, which is universally used
 464 as a joint material for hip joint replacement and is one
 465 of the best materials for biomedical applications,
 466 possessing good wear resistance, mechanical
 467 properties, and biocompatibility, is investigated
 468 (Chyr e at al., 2014).

469 Laser interference lithography uses an interference
 470 pattern produced by two or more coherent laser
 471 beams to pattern a material. The LIL mode is a
 472 superposition of the electric field vectors of the
 473 interfering beams, and highly patterned depressions
 474 or lines can be produced on the material surface using
 475 interference patterns. Compared with other methods,
 476 LIL has advantages such as relatively short process
 477 time, easy setup, high resolution, no surface
 478 contamination, flexible configuration and large
 479 working distance, which allows inexpensive,
 480 efficient and large area creation of three-dimensional
 481 micro- and nanostructures on biomaterials, and the
 482 intrinsic biocompatibility of the materials used to
 483 create the structures is not altered by laser treatment
 484 (Mattei e at al., 2014).

485 Studies (Wei e at al., 2016; Wang e at al., 2013; Mattei e
 486 at al., 2011; Gao e at al., 2012; Chyr e at al., 2014) show
 487 that surface texturing can significantly reduce
 488 friction in artificial joints. However, in addition to the
 489 labor-intensive procedures and complex processes
 490 currently used, it is still quite challenging to ensure
 491 the long-term use of artificial joints in terms of low
 492 friction, biocompatibility, and high wear resistance.

493 **5. Finishing processes of metal**
 494 **elements of hip joint**
 495 **endoprostheses**

496 When developing medical devices, especially in the
 497 field of endoprosthetics, such products are subject to
 498 increased requirements, including high strength,
 499 wear resistance, high machinability of alloys, as such
 500 products should have a smooth mirror surface, which
 501 in turn reduces abrasion of implants and thus extends
 502 their service life. However, the most important
 503 requirement for bioimplants is biocompatibility. The
 504 reason for this is the direct purpose of such products:
 505 installation and operation of endoprostheses inside
 506 the human body, which is necessary to replace
 507 damaged, destroyed or missing body parts for any
 508 reason.

509 Co-Cr-Mo based alloys have been found to have
 510 good mechanical properties: high resistance to
 511 fatigue (400-450 Nlmm²), corrosion resistance in
 512 aggressive media, wear resistance, ductility and
 513 strength (tensile strength of at least 1000 Nlmm²)
 514 and, as one of the main requirements, excellent
 515 biocompatibility. In addition, alloys of this type have
 516 a high resistance to deformation over time (Jenko e at
 517 al., 2018; Giacchi e at al., 2011; Ghalme e at al., 2016).
 518 Therefore, it can be concluded that the metal
 519 elements of endoprostheses made of this type of
 520 alloys meet the requirements for them.

521 Table 2 shows the generalized composition of Co-Cr-
 522 Mo alloy with applied components that take into
 523 account the addition of various alloying elements
 524 such as Mo, Ni, Ti, W and others.

525 **Table 2 - Table 2 - Content of components used in Co-**
 526 **Cr alloys [1-22]**

Components	Co	Cr	Mo	C	Si	Mn	N	Fe	W	Ni	P	S	Ti	Al	B
	The range	53-69	25-32	2-11	0.007-0.35	0.15-1.25	0.15-1	0.025-0.25	0.025-1	0.2-0.4	0.1-2.5	0.02-0.15	≤0.01	0.1-6	≤0.1

527 It is important to emphasize that no material in its
 528 pure form can meet all the requirements, so to
 529 improve the properties, structure and surface

530 modification is often used to enhance the surface
531 properties, thereby improving the tribological
532 properties of metal elements of hip arthroplasties
533 including hip joints.

534 Based on the literature review, the most commonly
535 used technology for heat treatment of hip joint
536 endoprostheses is aging at 900-1200 °C followed by
537 quenching or aging.

538 As a result of the research, as well as their
539 implementation in the technology of manufacturing
540 and processing of medical devices, not only the basic
541 properties of endoprostheses, including surface
542 quality, are improved, but also contribute to the
543 increase of tribological properties and service life of
544 the manufactured endoprostheses. In addition,
545 important advantages of Co-Cr-Mo alloys,
546 compared, for example, with titanium alloys, are also
547 their technological properties: high liquid-fluidity
548 (possibility of obtaining castings of very complex
549 geometry) and high quality of polishing after surface
550 finishing.

551 To date, various studies have been conducted on the
552 fabrication of metallic elements of endoprostheses.
553 The most attention is paid to biocompatibility,
554 durability, wear resistance, and corrosion resistance.

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