

the basis of which is an elastic metal frame attached to a tissue covering. Self-expanding 36

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stentgrafts, when installed in an artery, independently acquire the desired shape, moving 37 into it from the compressed state in which they are located in the introducer of the delivery 38 system. They use the effect of thermal shape memory, that is, they expand when released 39 from the delivery system into an area with a temperature above 30  $^{\circ}$ C. They are made 40 from nitinol (titanium nickelide), which, depending on heat treatment, can have various 41 properties, including shape memory and unique elastic properties. To form spatial 42 structures from nitinol wire, heat treatment is needed to fix the required shape. The heat 43 treatment mode determines the temperature at which nitinol is in a state of superelasticity, 44 that is, it recreates the shape specified during heat treatment. The Science and technology 45 park of BNTU "Polytechnic" has established serial production of stentgrafts, the design 46 of which contains zigzag elements made of nitinol (Figure 1). 47



Figure 1 – Nitinol stent element. 49

While developing the technology for forming the shape of elements, postoperative control 50 of zigzag elements for stentgrafts was carried out at a given temperature. It was found that 51 zigzag elements created on the same device and under the same thermal conditions can 52 have different bending stiffness and in a number of cases it turns out that the rigidity is 53 insufficient for use in stentgrafts. 54

The purpose of the study is to find ways to solve this problem. 55

## **2. Literature Review:** 56

Previously, the authors developed technological processes for the manufacture of stent 57 elements from nitinol wire, and they are known from literature sources (Rubanik, 2018). 58 It is known that for structures obtained from flexible wire, the following work is required: 59 preparation (cutting) of nitinol wire, connecting the ends of the wire by crimping a 60 stainless steel tube or welding, forming the wire in a device (to facilitate forming, the wire 61 is cooled to a temperature of approximately 5...15  $^{\circ}$ C), heat treatment (holding in an 62 furnace at a given temperature for a given time), assessment of the mechanical 63 characteristics of the obtained samples at fixed temperatures, installation in a delivery 64 system. The individual stages of the technological process are described in various 65 published works. In particular, forming processes are described in (Utela et al., 2007), 66 (Hodgson, 2000), processes for joining wire ends by laser welding (Kush & Kapil, 2019), 67 and heat treatment processes in (Ming, 2001). The authors carried out a number of studies 68 (Minchenya, Savchenko & Gitkovich, 2010; Savchenko, Minchenya V. & Minchenya N., 69

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2012; Khrustalyov et al., 2013; Minchenya & Savchenko, 2014; Minchenya et al., 2015, 70 2016, 2017, Ulasevich, Savchenko & Minchenya, 2022; Savchenko et al., 2022), which 71 resulted in the production of zigzag elements for stentgrafts and other medical products 72 from nitinol wire. 73

However, in real production conditions, the undesirable effect described above appeared, 74 this is a change in rigidity in a separate part of the zigzag element, which can be caused 75 by the following reasons:  $\frac{76}{20}$ 

– uneven heating and cooling of the wire during heat treatment due to multilayer winding; 77

– uneven wire tension when winding a zigzag element on a tubular device for the same 78 reason; 79

– change in dimensions and, accordingly, a decrease in rigidity due to the transition to a 80 new layer of winding; 81

– change in tension due to the difference in the coefficients of thermal linear expansion 82 of nitinol and the material of the device. 83

For heat treatment, stent elements are placed on multi-site devices in the form of tubes 84 with pins to give the wire a zigzag shape. To increase productivity, the wire is wound in 85 several rows (e. g., 2 rows), each row in several layers (the number of layers reaches ten). 86 The appearance of such a device is shown in Figure 2., the location of the wire on the pins 87 is in Figure 3. 88



Figure 2 – Wire winding mandrel. 90

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To create identical conditions in the process of forming shape memory, several zigzag 114 samples with different tensions were simultaneously installed on the mandrel, which, 115 together with the device, were subjected to heat treatment. After this, the samples were 116 removed and subjected to stiffness measurements in a device that made it possible to 117 measure the deformation force of the samples at a given angle, in this case  $30^{\circ}$  (Fig. 5). 118



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Figure 5 – Measuring device. 120

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121 **4. Results and Discussion:** 122 The results of measuring the hardness of heat-treated samples are given in Table 1. 123 **Table 1 – Deformation force depending on the tension force, N** 124 0 5 10 30 50 70 90 1,7 1,5 1,4 1,2 0,95 0,7 0,45 It can be seen that as the tension increases, the stiffness of the samples decreases. For 125

clarity, this is shown in the graph (Figure 6). 126



Figure 6 – Dependence of sample rigidity on tension during heat treatment. 128

The technological features of the heat treatment process do not allow it to be carried out 129 with zero wire tension, since it is difficult to achieve the required shape. (Utela et al., 130) 2007) suggest using special 3D-printed fasteners, but this can cause difficulties in 131 ensuring uniform heating and cooling. When winding, it is necessary to ensure the same 132 tension on all zigzag branches in order to ensure the same rigidity of the elements as a 133 result. To achieve this, some changes to the design of the devices are proposed. In 134 particular, it is proposed to use fewer layers of winding and change the mechanics of 135 tension. These measures should lead to a reduction in friction between the wire and the 136 elements of the fixture and, therefore, increase the uniformity of tension. 137

At the same time, the results obtained require clarification: whether the increase in the 138 bending rigidity of the wire with a decrease in tension is the result of the nature of the 139 heat treatment or an increase in the bending radius due to a decrease in effort. According 140 to the calculation results, the determining factor is still the influence of heat treatment 141 conditions. 142

In addition, the following factors should be considered. 143

The coefficient of thermal linear expansion of nitinol is from  $6.6 \cdot 10^{-6}$  1/ $\degree$ C in the 144 martensitic phase to  $11.10^{-6}$  1/°C in the austenitic phase. For stainless steel 40X13, the 145 same figure is obviously higher -  $12,5.10^{-6}$  1/ $\degree$ C. That is, when heated, the tension of the 146 wire will increase due to temperature deformations. This should be taken into account 147 when selecting pretension. 148

When switching to a new layer of winding, the diameter of the resulting workpiece will 149 increase by double the diameter of the wire. For the study, wire samples with a diameter 150 of 0.45 mm were taken, that is, the diameter from layer to layer will increase by 0.9 mm. 151

When moving to a new layer, each time the length of the inclined section of the zigzag 152 will increase by approximately 1.3%, respectively, the bending rigidity of this section will 153 decrease by the same amount. By the tenth layer the elongation will be 12%. 154

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Even if you connect the ends of the stent element blank to obtain the same diameter, the 155 zigzag geometry will still be different, which will lead to a difference in the stiffness of 156 the finished stent element. Moreover, when using a blank from layer to layer, the 157 unevenness of the rigidity of the finished stent element in different directions will 158 increase. Therefore, it is necessary to maintain uniform tension of the zigzag around the 159 circumference of the stent element. 160

## **5. Conclusion:** 161

It is necessary to change the design of the heat treatment device to ensure wire fixation 162 and uniform zigzag around the circumference of the stent element with minimal wire 163 tension. 164

When choosing the wire tension force, it is necessary to take into account the coefficients 165 of thermal linear expansion of nitinol and the mandrel material. 166

The results obtained will be proposed for implementation in the technological process of 167 manufacturing medical products from nitinol in the Scientific and Technological Park of 168 BNTU "Polytechnic". After production tests, conclusions will be drawn about the 169 advisability of using them in production conditions. 170

